

Comparison between different configurations of Hybrid Raman/Erbium-Doped Fiber Amplifiers

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Purposes of the Work

- ▶ Why Hybrid Raman/Erbium-Doped Fiber Amplifiers ?
- ▶ The *Non-Linear Weight*: comparison of HFA configurations.
- ▶ Definition of a general multi-span system structure.
- ▶ A closed form analysis providing the maximum reachable distance vs. the span length, given a target *OSNR* and *Non-Linear Weight*.
- ▶ Description of the design process using the described analysis and simulation results.
- ▶ An example: design of 32 x 40 Gbit/s NRZ system in the C bandwidth.

Why Hybrid Amplification?

Pros Raman vs. EDFA

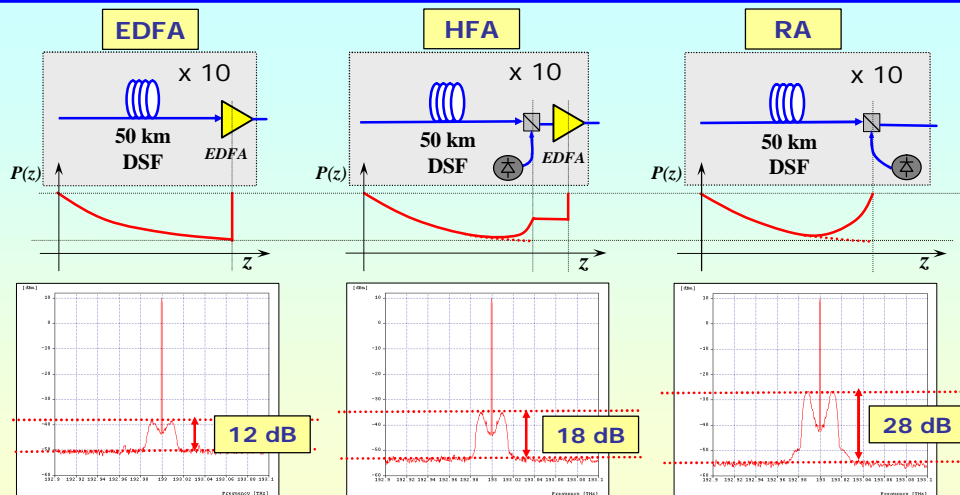
- ▶ Distributed amplification
- ▶ Lower amount of ASE noise
- ▶ Larger bandwidth
- ▶ Gain-shape can be designed
- ▶ Theoretically available in S, C, L bandwidth
- ▶ Allow to enlarge the fiber-span
- ▶ Easier upgrade of installed systems

Cons Raman vs. EDFA

- ▶ High gain -> high propagating power
- ▶ Rayleigh scattering may limit performance
- ▶ X-talk signal-pump-signal (in co-prop scheme)
- ▶ No saturation working-mode in order to define output power
- ▶ Same input power -> Higher impact of non-linearity

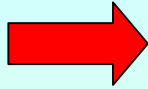


Non-Linear Impact: EDFA vs. RA



Using the same transmitted power ($P_{TX}=10$ dBm) different configurations of HFA can not be directly compared

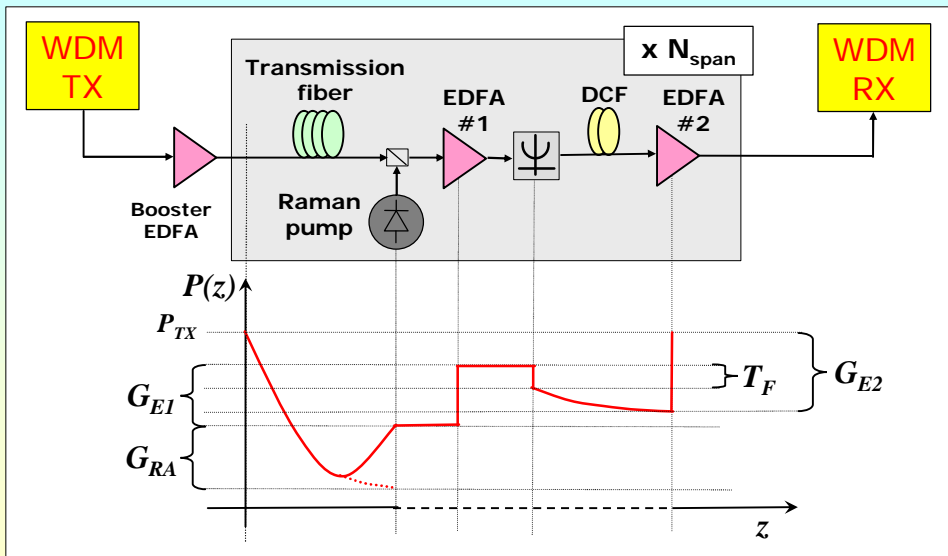
Non-linear weight definition



$$K_{NL} = \int_0^{L_{link}} g(z)P(z)dz \quad [\text{rad}/\text{ch}]$$

It is the overall non-linear phase-shift that one channel experiences along the system.

It allows to compare systems based on the same modulation format, number of channels and channel spacing, and using the same fiber. Total link lengths may be different as well as the span lengths.



Transparency condition

$$G_{TOT} = G_{RA,dB} + G_{E1,dB} + G_{E2,dB} = \mathbf{a}_{S,dB} L_{span} + T_{F,dB} + \mathbf{a}_{DCF,dB} L_{DCF}$$

G_{TOT} is defined but individual gains are undetermined

Definition of gain values through parameters
 k_1 and k_2 is the goal of the process

$$k_2 = \frac{G_{RA,dB} + G_{E1,dB}}{G_{TOT}}$$

Sets the amount of gain of the HFA made by RA+EDFA#1 and of EDFA#2 . Controls the input power of the DCF.

$$k_1 = \frac{G_{RA,dB}}{G_{RA,dB} + G_{E1,dB}} = \frac{G_{RA,dB}}{k_2 G_{TOT}}$$

Defines individual gains of RA and EDFA#1 .

OSNR at the end of the considered optical link

$$OSNR = \frac{P_{TX}}{hfB_O N_{span} \left[\left(n_{eq,RA} + n_{sp,E1} \frac{G_{E1} - 1}{G_{E1} G_{RA}} \right) \exp(+\mathbf{a}_S L_{span}) + n_{sp,E2} (G_{E2} - 1) \right]}$$

We use the *Non-Linear Weight* in order to compare configurations with different parameters: individual gains, span length, total length.

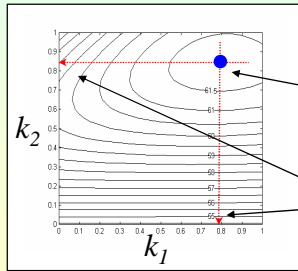
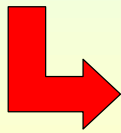
$$P_{TX} = \frac{k_{NL}}{N_{span} [\mathbf{g} L_{eff} + \mathbf{g}_{DCF} \exp(-\mathbf{a}_S L_{span}) G_{RA} G_{E1} T_F L_{eff,DCF}]}$$

$$OSNR = \frac{k_{NL} P_1}{N_{span}^2 N_1} = \frac{k_{NL}}{N_{span}^2} OSNR_1$$

Value of P_{TX} which makes $k_{NL} = 1$ after only one span

Amount of noise entering the system every span

For each L_{span}

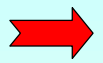


$$OSNR_1^{opt} = \max\{OSNR_1\}$$

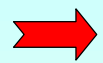
$$(k_1, k_2)_{opt}$$

$$G_{RA}^{opt}, G_{E1}^{opt}, G_{E2}^{opt}$$

$$L_{span}$$



$$OSNR_1^{opt}$$



$$G_{RA}^{opt}, G_{E1}^{opt}, G_{E2}^{opt}$$



$$L_{max} = \text{int} \left\{ \sqrt{\frac{k_{NL}^{max}}{OSNR_{min}}} OSNR_1^{opt} \right\} L_{span}$$



$$L_{max} = f(L_{span})$$

given $k_{NL}^{max}, OSNR_{min}$



$$L_{max} = f(k_{NL}^{max})$$

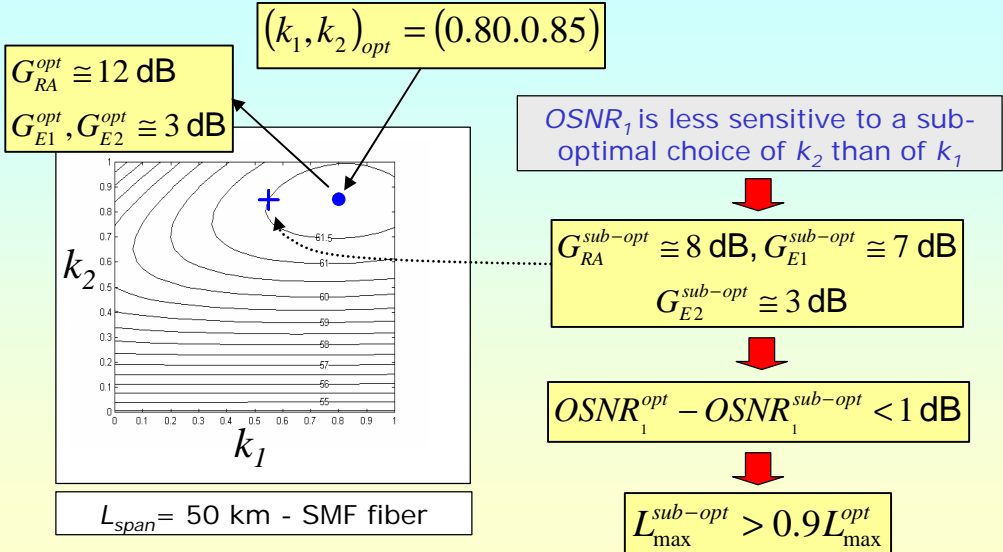
given $L_{span}, OSNR_{min}$



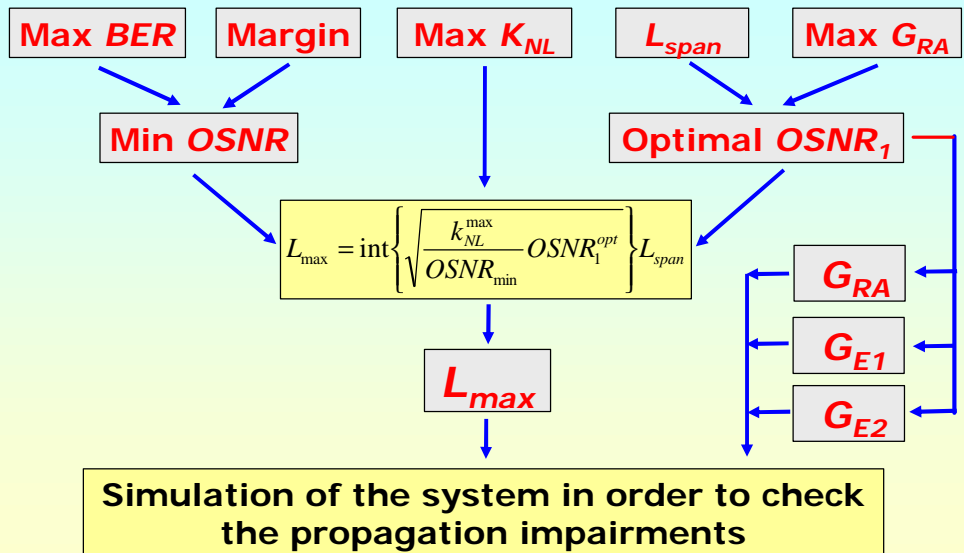
$$L_{max} = f(OSNR_{min})$$

given k_{NL}^{max}, L_{span}

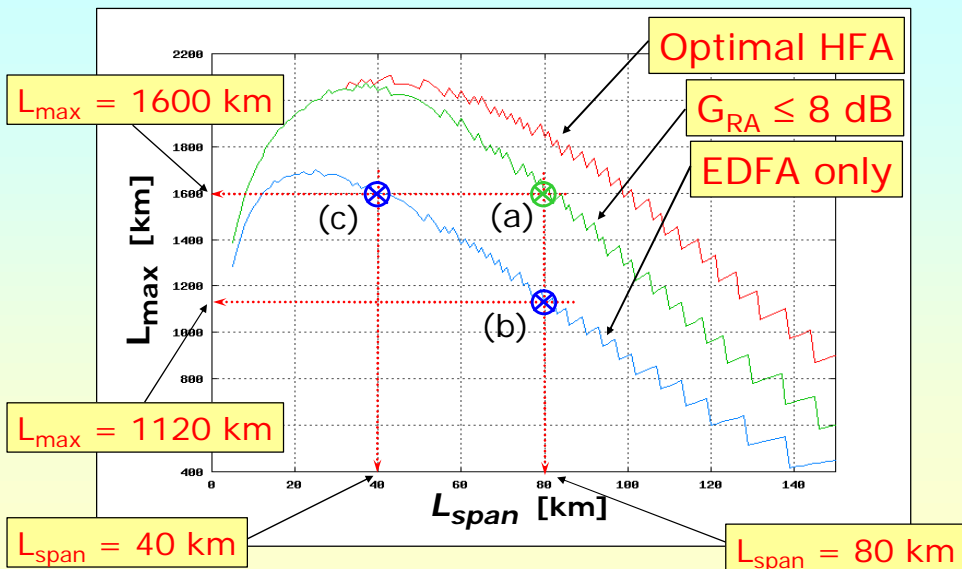
Contour plot of $OSNR_1$ in the (k_1, k_2) space



The Design Process



- ▶ 32 x 40 Gbit/s NRZ channels, 100 GHz spaced
- ▶ Transmission fiber: $D=5$ ps/nm/km, $A_{eff}=55 \mu\text{m}^2$
- ▶ DCF: $D=-100$ ps/nm/km, $A_{eff}=25 \mu\text{m}^2$
- ▶ Dispersion perfectly compensated at the receiver
- ▶ Raman amplification: two-pump with $G_{RA} < 8$ dB
- ▶ EDFAs: flat gain and $NF=4.5$ dB
- ▶ GFF loss: 2 dB
- ▶ Target OSNR: 15 dB over 0.5 nm \Rightarrow BER $< 10^{-9}$ \Rightarrow using FEC RS(255,239) \Rightarrow 3 dB margin to get BER $< 10^{-12}$
- ▶ **Goal:** maximum reachable distance with pseudo-linear propagation ($k_{NL}=0.25$ rad/channel)



HFA, $G_{RA} \leq 8$ dB

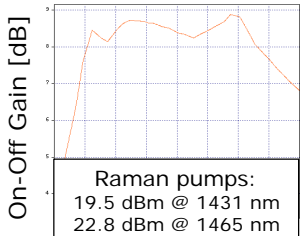
EDFA only

(a)

$P_{TX} = -5.6$ dBm/ch
 $L_{span} = 80$ km
 $L_{TOT} = 1600$ km
 $G_{RA} = 8$ dB
 $G_{E1} = 8$ dB
 $G_{E2} = 4$ dB

$P_{TX} = -2.9$ dBm/ch
 $L_{span} = 80$ km
 $L_{TOT} = 1120$ km
 $G_{E1} = 12$ dB
 $G_{E2} = 8$ dB

(b)



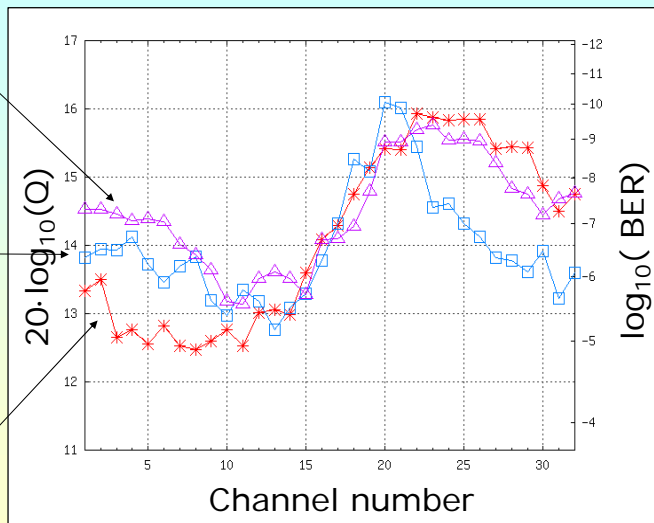
$P_{TX} = -7.1$ dBm/ch
 $L_{span} = 40$ km
 $L_{TOT} = 1600$ km
 $G_{E1} = 8.8$ dB
 $G_{E2} = 2.2$ dB

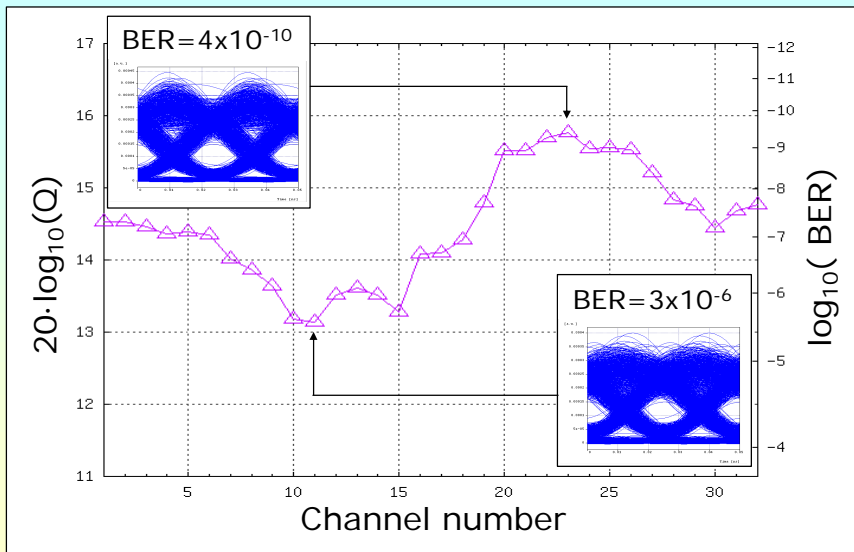
(c)

HFA
20 x 80 km

EDFA
40 x 40 km

EDFA
14 x 80 km





- ▶ It has been derived a closed-form analysis giving the maximum reachable distance using the optimal HFA.
- ▶ A design process for HFAs has been described for DWDM systems.
- ▶ The design process has been applied to a 32 x 40 Gbit/s NRZ system.
- ▶ Results demonstrate:
 - ▶ non-linear weight is a good parameter for comparison of different system configurations;
 - ▶ use of HFAs enlarge the maximum reachable distance.
- ▶ Further investigation: simultaneous optimization of HFA and dispersion map.